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**International Union of Crystallography  
Commission on Crystallographic Apparatus  
Single-Crystal Intensity Measurement Project Report  
II. Least-Squares Refinements of Structural Parameters**

BY WALTER C. HAMILTON

*Brookhaven National Laboratory, Upton, New York 11973, U.S.A.*

AND S. C. ABRAHAMS

*Bell Telephone Laboratories, Inc., Murray Hill, New Jersey 07974, U.S.A.*

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The structure factors measured by the participants in the single-crystal intensity project of the I.U.Cr. Commission on Crystallographic Apparatus on D(+)-tartaric acid have been used in least-squares refinement of the structural parameters. The structure factors submitted by each participant were subjected to two refinements – once with heavy atoms only and once with all atoms including hydrogen. The parameters resulting from these refinements differ by magnitudes which suggest that the estimated standard deviations of the positional parameters obtained in the least-squares refinements are not infrequently a factor of about two too small and about  $\sqrt{2}$  too small on the average. The agreement for the thermal vibration parameters may be even worse – by an additional factor of about two. These results are consistent with the indications of serious systematic errors in some of the experiments revealed in part I of this report. A modal group of six experiments with good interexperimental agreement leads to least-squares refined position parameters that are also in fair agreement; the maximum value of the ratio of the externally estimated standard deviation to the internal estimate from the least-squares refinements is about 2.5. The finding that results of possible high precision but low accuracy are not uncommon in single crystal-structure investigations is confirmed.

### Introduction

In part I of this report (Abrahams, Hamilton & Mathieson, 1969), later referred to as part I, the interexperimental agreement factors and classical analysis-of-variance techniques have revealed the presence of systematic errors in many diffractometer experiments. Such errors cause differences between relative structure factors, measured by different experimenters on different specimens of the same substance, to be much larger than the internal consistency of the individual experiments would suggest. The analysis-of-variance techniques used in part I are appropriate for revealing the nature of the systematic differences among experiments without recourse to a theoretical model. Nevertheless, it is of interest to examine the results of applying the usual least-squares refinement procedure to the

structure factors to determine how the possible systematic errors are manifested in the refined positional and thermal parameters.\*

### Refinement procedure

Each set of structure factors was subjected to least-squares refinement, using the usual model for the oxygen and carbon atoms that

$$F(hkl) = K \sum_j f_j \exp [2\pi i(hx + ky + lz)] \exp [-\sum_{ik} h_i h_k \beta_{ik}]$$

\* Since limited data sets consisting of no more than 332 independent reflections were used, none of the results below should be taken as definitive determinations of the average parameters in the D(+)-tartaric acid structure, especially since the reflections used extended only to  $\sin \theta/\lambda = 0.5 \text{ \AA}^{-1}$ .

and replacing the anisotropic thermal vibration term by  $\exp\{-B(\sin\theta/\lambda)^2\}$  for the hydrogen atoms, where  $\{h_i: i=1, 2, 3\}$  is identical to  $\{h, k, l\}$ . The parameters refined were the overall scale factor  $K$  and, for each atom,  $x, y, z$  and  $\{\beta_{ik}: i=1, 3; k=1, 3\}$  or  $B$  for hydrogen atoms. Free-atom atomic scattering factors were used for all atoms (*International Tables for X-ray Crystallography*, 1962); no corrections were made for anomalous scattering (which is small). The space group was assumed to be  $P2_1$  (Stern & Beevers, 1950). The numbering of the atoms is presented in Table 1 and agrees with that used by Okaya, Stemple & Kay (OSK, 1966) in the most recent published refinement of this structure. The heavy atom parameters of OSK were used as initial values in the full matrix least-squares refinements (Busing, Martin & Levy, 1962). The quantity minimized was  $\Sigma w(|F_{\text{obs}}| - |F_{\text{calc}}|)^2$ , where the weight  $w$  was assumed equal to  $(0.1|F_{\text{obs}}|)^{-2}$ .\* For each set of data an attempt was made to carry out two refinements, one with the ten heavy atoms only, and one including hydrogen atoms. In the latter case, the initial hydrogen atom parameters were taken from some preliminary neutron diffraction results of Cox, Sabine & Taylor (1966). In all the refinements, the  $y$  parameter of atom 1 was held fixed at 0.0343 – the final value of OSK; this is possible because of the one degree of freedom in the choice of origin in this space group.

Table 1. Atom numbering scheme

	Number		Number
O(1)	1	C(3)	9
O(2)	2	C(4)	10
O(3)	3	H(1)	11
O(4)	4	H(2)	12
O(5)	5	H(3)	13
O(6)	6	H(4)	14
C(1)	7	H(5)	15
C(2)	8	H(6)	16

## Results

In Table 2 are presented the results of the heavy atom refinements.† Since experimenters 6 and 10 supplied one zone of data only, it was not possible to refine these data sets. (There was in fact insufficient data from these two experiments for an anisotropic two-

\* This weighting formula was found to be suitable by an analysis of the average value of  $\Delta F/\sigma$  as a function of  $F$ . There were few reflections of low enough intensity to be overweighted by this formulation.

† It was not possible to refine the data for experiment 11b to a satisfactory solution. Non-positive-definite thermal parameters were obtained, and the convergence procedure became unstable, the agreement factor getting suddenly worse and then better. This was possibly due to the small number of independent structure factors that was available for this data set. Nevertheless, a set of parameters for this experiment is included in Table 2; this set corresponds to the lowest value for the agreement ratio obtained during the refinement procedure. The omission of this experiment from the analysis presented in Table 2 did not affect any of the conclusions.

dimensional refinement.) The parameters ( $P$ ) are numbered in the order  $x, y, z, \beta_{11}, \beta_{22}, \beta_{33}, \beta_{12}, \beta_{13}, \beta_{23}$ . Table 2 contains the following data:

(i) In the last fifteen columns are the parameters  $P_i$  obtained from the individual refinements; the least-squares estimated standard deviations are not given but may be inferred from the standard deviation of the mean (see  $\sigma$  below).

(ii) The MAXIMUM and MINIMUM of the fifteen parameter values obtained.

(iii) The mean parameter value (labelled AVERAGE) defined by

$$\mu = \sum_i \left( \frac{P_i}{\sigma_i^2} \right) / \sum_i \left( \frac{1}{\sigma_i^2} \right)$$

where  $\sigma_i^2$  is the estimated variance of the parameter from the least-squares refinement obtained in the usual way from the inverse matrix of the normal equations by multiplication by the goodness-of-fit parameter  $\Sigma w(\Delta F)^2/(n-m)$ .

(iv) The parameter value reported by OSK (1966) for the X-ray refinement.

(v) The estimated standard deviation of the weighted mean based on the agreement among the experiments:

$$\sigma_{\text{EXT}} = \left[ \frac{\sum_i \frac{(P_i - \mu)^2}{\sigma_i^2}}{(n-1) \sum_i \frac{1}{\sigma_i^2}} \right]^{1/2}$$

(vi) The estimated standard deviation of the mean based on the individually estimated standard deviations:

$$\sigma_{\text{INT}} = \left[ \sum_i \frac{1}{\sigma_i^2} \right]^{-1/2}.$$

(vii) The variance ratio

$$\text{RATIO} = (\sigma_{\text{EXT}}/\sigma_{\text{INT}})^2.$$

In the absence of systematic error RATIO is expected to have, on the average, a value close to unity. Except for the variance ratio, all numbers in Table 2 have been multiplied by  $10^5$ .

In Table 3 are presented similar results for the refinements which include the six hydrogen atoms. The fourth parameter for each hydrogen atom is the isotropic thermal parameter  $B$ . The data of experiments 1, 3, 12 and 14 did not lead to successful refinements; the positional and thermal parameters of the hydrogen atoms varied widely, and the refinements diverged. (It is possible that careful individual analysis in each of these cases would have led to non-divergent refinement. We note here only that a routine refinement starting from the initial neutron diffraction values was not possible for these four experiments, as it was for the others.) These experiments are thus omitted from Table 3.

As a further summary of the refinements, we present in Table 4 the values of the agreement ratios

$$R = \Sigma ||F_{\text{obs}}| - |F_{\text{calc}}|| / \Sigma |F_{\text{obs}}|,$$

$$wR = [\Sigma \{w^{1/2}(|F_{\text{obs}}| - |F_{\text{calc}}|)\}^2 / \Sigma (w^{1/2}|F_{\text{obs}}|)^2]^{1/2}.$$

In addition, for the heavy atom refinements, typical values of the least-squares estimated standard deviations ( $\sigma$ ) for the  $x$ -positional parameter are also quoted.

## Discussion

It will be left for the reader to analyze the variation among the parameter sets in detail, but some conclusions will be given here. The results of the refinements confirm the conclusions of part I. There are systematic

differences among the experiments. Again this is most obvious for experiment 13, where  $\beta_{33}$  is about a factor of four larger than the average value of  $\beta_{33}$  obtained over all experiments; a systematic error as a function of  $l$  is thus clearly indicated. Despite this great discrepancy, the  $R$ ,  $wR$  and  $\sigma(x)$  values (see Table 4) for this experiment are comparable with those for the other experiments.

The most important figures in Tables 2 and 3 are the variance ratios  $\sigma_{\text{EXT}}^2 / \sigma_{\text{INT}}^2$  (RATIO). In the absence of systematic error, these quantities should be distributed with a mean of approximately 1.0 and variance approximately  $\{2(n-1)\}^{1/2}$  where  $n$  is the number of experiments compared. Inspection of Table 2 reveals a maximum value of 4.3 for a position coordinate and 35.7 for a thermal vibration parameter. The corre-

Table 2. Results of heavy atom refinements of the project data

The atom numbering scheme is given in Table 1, and explanation of the contents of the Table is given in the text. For fifteen degrees of freedom, values of RATIO exceeding 1.66 are significant at the 95% level.

ATOM	P	MAXIMUM	MINIMUM	AVERAGE	DSK	SIGMA(EXT)	SIGMA(INT)	RATIO	1	2	3	4	5	7	8	9	11A	11B	12	13	14	15	16	
1	1	33941	33174	33747	33820	28	16	0	2.0006	33941	33798	33174	33831	33726	33798	33805	33808	33707	33460	33500	33707	33807	33546	33775
1	1	3430	3410	3430	3430	0	0	0.0000	3430	3430	3430	3430	3430	3430	3430	3430	3430	3430	3430	3430	3430	3430	3430	
1	3	51635	50707	51057	51020	42	24	3.1206	51162	51179	51635	51060	50963	51047	51138	51006	50940	51313	51649	50950	51071	50701	51038	
1	4	2462	476	826	665	61	26	5.9485	1626	1626	1626	1626	1626	1626	1626	1626	1626	1626	1626	1626	1626	1626	1626	
1	5	2469	1968	2355	954	54	36	3.0118	2158	1035	1736	1626	2054	1734	1249	2143	2357	1363	1364	2469	2176	1948	1826	
1	6	5850	-961	1199	1149	262	55	22.3950	1466	670	1618	1047	1183	951	1342	549	1002	1452	-961	5850	1146	1421	1093	
1	7	374	-271	26	-2	29	34	-4.9766	-136	4	243	8	21	53	120	23	176	119	141	313	258	271	253	
1	8	466	-412	238	284	21	27	-6.0165	180	272	252	180	272	180	272	252	180	272	180	272	180	272	180	
1	9	771	42	341	493	43	50	-7.0474	60	106	116	42	420	309	179	240	275	423	249	771	647	259	405	
2	1	43610	42896	42988	42960	21	15	1.9898	4165	42967	41865	42905	42941	42945	43012	43004	43127	43610	43362	42960	42896	43008	43046	
2	2	-3101	-3804	-3182	-3249	41	50	1.1102	-3095	-3539	-3616	-3405	-3460	-3593	-3106	-3406	-3145	-3804	-3379	-3472	-3101	-3325		
2	3	-1921	-2610	-2140	-2189	25	24	1.0485	-2169	-2465	-2239	-2114	-2113	-2207	-2104	-2105	-2141	-1921	-2050	-2141	-2050	-2111		
2	4	-122	-122	-122	-122	51	54	2.0445	-1965	-2050	-1965	-1965	-1965	-1965	-1965	-1965	-1965	-1965	-1965	-1965	-1965			
2	5	3034	1511	2345	2113	91	66	1.9250	1927	1511	2864	2301	2590	2135	2153	1963	3034	2141	2549	2230	2478	2172		
2	6	6736	-779	1139	1412	246	53	21.5111	682	1282	1074	1009	1249	1483	1063	6736	-779	6078	931	1615	967			
2	7	583	-193	380	160	33	38	-2.0540	303	303	303	303	303	303	303	303	303	303	303	303	303			
2	8	386	-204	294	-407	10	50	-3.0548	380	172	159	229	325	325	386	320	370	59	258	143	254	231		
2	9	-27	-1730	-220	-207	50	50	-9.747	-397	-165	-883	-343	-161	-142	-275	-165	-224	-170	-195	27	-424	-146		
3	1	61120	60840	60955	60940	18	16	1.1340	60914	60843	60993	60840	60956	60979	60908	60883	61075	61420	60873	61060	60978	60966		
3	2	3499	2928	3010	3007	28	42	1.4305	305	410	305	305	305	305	305	305	305	305	305	305	305	305		
3	3	1230	86	490	490	26	24	1.0485	3094	3094	3094	3094	3094	3094	3094	3094	3094	3094	3094	3094	3094			
3	4	2681	960	1778	2374	98	64	2.3546	960	1010	2073	1737	1944	1648	1299	1831	2681	2165	2153	2202	2100	1570		
3	5	437	-193	40	116	30	30	-1.9770	162	162	162	162	162	162	162	162	162	162	162	162	162			
3	6	546	-76	175	303	25	32	-5.0994	546	98	306	191	121	16	258	207	-76	392	104	120	275	140		
3	7	861	34	271	440	41	47	-7.0607	194	327	861	410	333	292	233	34	114	589	273	173	241	536		
4	1	30852	30244	30729	30630	14	16	-8.063	30494	30852	30763	30763	30754	30733	30705	30704	30730	30730	30726	30698	30751	30767		
4	2	4121	4121	4121	4121	44	37	-2.0450	3153	4125	4125	4125	4125	4125	4125	4125	4125	4125	4125	4125	4125			
4	3	23826	22476	23553	23350	33	25	1.7105	23211	23528	23599	23547	23567	23540	23574	23576	23579	23579	23564	23563	23598	23547		
4	4	1567	220	572	648	38	26	2.4743	3243	352	645	645	645	645	645	645	645	645	645	645	645			
4	5	18216	17592	17854	17900	43	51	1.9741	17516	17716	17954	1792	17776	17783	17623	18284	18784	18759	18759	18759	18759	18759		
4	6	3427	1987	2520	2688	94	77	1.4700	3427	2079	2079	3205	3205	2661	2657	2954	2954	2985	2981	1987	2378			
4	7	7841	-214	214	2362	275	54	25.4250	1504	1355	2775	1380	2056	1949	1765	2663	2477	7841	-24	6705	1879	2289		
4	8	38	-105	29	31	45	45	-1.9770	162	162	162	162	162	162	162	162	162	162	162	162	162			
4	9	616	-135	406	511	30	37	-1.7606	509	321	-376	605	489	476	337	334	460	151	-61	310	378	612		
4	10	-116	-1254	-881	-861	37	37	-3.9557	-1254	-94	-878	-878	-878	-930	-928	-825	-553	-652	-892	-648	-1042	-764		
5	1	-7550	-8018	-7750	-7649	26	18	1.2113	-8001	-7704	-7722	-7674	-7722	-7722	-7722	-7722	-7722	-7802	-7802	-7802	-7802	-7802		
5	2	8341	7719	7926	7920	43	45	9.9305	8260	7802	7753	7753	7805	7767	8162	7972	8341	7805	8103	7719	8168	8060		
5	3	34824	17592	17854	17900	43	51	1.9741	17516	17716	17954	1792	17776	17783	17623	18284	18784	18759	18759	18759	18759			
5	4	3427	1987	2520	2688	94	77	1.4700	3427	2079	2079	3205	3205	2661	2657	2954	2954	2985	2981	1987	2378			
5	5	7841	-214	214	2362	275	54	25.4250	1504	1355	2775	1380	2056	1949	1765	2663	2477	7841	-24	6705	1879	2289		
5	6	3427	-257	-59	-1	22	45	2.4702	-94	-118	-69	-257	-138	-88	-65	-47	176	6	116	7	-206	-10		
5	7	870	-861	403	194	42	42	-2.5900	42	-101	-296	-102	-124	-143	-102	-124	-143	-142	-96	-205	-227	-110		
5	8	607	-1669	176	278	54	44	4.4916	-42	-160	-1669	166	337	311	183	-53	492	-961	-278	-145	-279	-227	-110	
5	9	687	-581	157	161	45	65	4.4940	231	196	393	21	20	208	-33	322	262	-581	371	116	-187	191		
6	1	25502	19702	20103	20310	32	23	2.0227	19005	20101	20070	20502	2013	20311	20288	19893	20502	20256	19792	20065	20110	20011	20705	
6	2	22511	22322	22578	22730	39	53	5.5508	2257	22454	22454	22322	22431	22550	22577	22870	22557	22577	22557	22577	22557	22557		
6	3	18144	15001	1792	18110	81	39	4.4781	1787	18025	18014	17963	17970	17880	17455	17951	15001	17627	18144	17898	17597	18144		
6	4	3427	-374	111	442	51	32	2.4269	2215	-86	-188	-56	238	276	155	-99	617	-374	348	262	-134	139		
6	5	1212	96	1212	1266	75	75	11.2256	40	997	1478	930	1184	1179	1046	1523	1431	1212	1212	1212	1212			
6	6	3427	-257	132	255	70	70	2.0458	102	102	102	102	102	102	102	102	102	102	102	102				
6	7	870	-861	403	194	42	42	2.2273	419	413	-861	322	496	439	870	658	-596	-595	102	558	55	298		
6	8	440	-689	-124	33	33	60	-6.0186	-526	-250	-250	-533	-681	-447	-519	-322	-382	-152	-40	-669	-118			
7	1	2517	1676	2216	2190	29																		

Table 3. Results of refinement of all atom parameters for the project data

Only those experiments which led to successful hydrogen atom refinements are included. For nine degrees of freedom, a value of RATIO greater than 1.88 is significant at the 95% significance level.

ATOM	P	MAXIMUM	MINIMUM	AVERAGE	OSK	SIGNAL(EXT)	SIGNAL(INT)	RATIO	2	4	5	7	8	9	11A	13	15	16	
1	1	31825	33618	33738	33820	15	15	1.0550	33715	33825	33735	33788	33780	33618	33711	33795	33721	33735	
1	2	3430	3430	3430	3430	0	0	1.0000	3430	3430	3430	3430	3430	3430	3430	3430	3430	3430	
1	3	5117	5000	51034	51020	21	20	1.1335	5117	5119	51049	5117	5117	51010	5117	51050	50922	50922	
1	4	889	304	1418	1415	39	33	1.2277	1415	1415	1415	1415	1415	1415	1415	1415	1415	1415	
1	5	2545	1035	1918	2355	101	45	4.8994	1355	1913	2069	1760	1347	1728	2421	2545	2003	1946	
1	6	5729	709	1108	1149	299	47	19.1066	709	893	1025	902	1270	1822	1302	5729	950	845	
1	7	73	-304	142	20	31	19	1.1933	-130	130	130	130	130	130	130	130	130	130	
1	8	456	133	282	284	21	26	1.7661	215	357	287	246	329	344	456	133	397	259	
1	9	681	-93	226	269	48	42	1.3100	-77	273	193	193	188	168	681	77	311	311	
2	1	4102	42570	42809	42960	31	16	3.6106	42420	42570	42728	42780	42714	42836	43002	42873	42910	42905	
2	2	-1096	-3757	-1343	-3249	40	33	1.4237	-3570	-3372	-3392	-3395	-3449	-3056	-3362	-3407	-3173	-3318	
2	3	-1180	-2378	-2145	-2189	38	26	2.1522	-1958	-2074	-2101	-2131	-2083	-2378	-1946	-1974	-1990	-2248	
2	4	-678	-100	-100	-100	49	34	1.3474	-100	-100	-100	-100	-100	-100	-100	-100	-100	-100	
2	5	3187	1857	2362	2713	112	58	3.6940	1857	2738	2687	2126	2466	1910	3187	2544	2776	2071	
2	6	6343	977	1436	1412	275	53	27.0927	1127	1646	1326	1205	1720	1533	977	6343	1495	1254	
2	7	71	15	186	33	31	1.1062	153	159	167	162	159	159	159	159	159	159	159	
2	8	409	261	477	-297	50	29	4.2057	50	50	50	50	50	50	433	309	321	321	
2	9	196	-580	-151	-298	68	44	2.3841	39	196	-14	-40	96	-580	-462	-65	-598	-186	
3	1	6028	60740	60859	60840	13	13	0.9967	60791	60787	60870	60890	60874	60740	60928	60912	60865	60856	
3	2	1129	105	665	500	74	35	4.4061	358	105	551	542	897	896	718	1129	725	725	
3	3	30111	29397	30091	30050	21	21	0.9534	30117	29995	30136	30118	30165	29937	30038	30171	30117	30117	
3	4	441	34	219	42	43	43	1.4747	42	34	34	34	34	34	34	34	34	34	
3	5	316	1102	2065	2374	95	55	2.9847	1102	1862	2163	1973	1450	2232	3106	2233	2301	2026	
3	6	6076	889	1514	1634	302	39	57.6759	889	1154	1318	1329	1176	2061	1067	6076	2196	1264	
3	7	75	17	20	20	26	30	2.8017	214	320	186	133	117	117	117	117	117	117	
3	8	150	-116	-110	-303	24	24	2.0088	191	190	151	127	167	167	167	167	167	167	
3	9	742	120	394	440	47	39	1.9945	431	517	501	403	334	269	120	204	742	260	
4	1	30847	30607	30716	30630	20	15	1.7910	30867	30827	30715	30725	30733	30798	30737	30662	30607	30669	
4	2	42479	41390	41814	41730	84	35	5.7912	41531	41390	41646	41726	41673	42008	42041	41643	42479	41893	
4	3	23643	23704	23431	23350	46	35	3.2664	23565	23342	23402	23439	23646	23603	23711	23004	23076	23384	
4	4	416	10	0	40	40	40	1.3456	40	40	40	40	40	40	40	40	40	40	
4	5	1853	847	1416	1708	73	51	2.0259	847	1417	1518	1275	1082	1500	1603	1702	1755	1286	
4	6	5087	322	820	1018	239	50	22.4216	322	592	501	717	925	1681	1794	5087	1367	758	
4	7	142	-185	-144	-199	18	30	3.3924	-12	-108	-94	-91	-29	-19	-19	-19	-19	-19	
4	8	534	146	146	140	40	24	2.0050	307	320	201	151	151	151	151	151	151	151	
4	9	394	-96	161	158	39	38	1.1028	-1438	-942	-1001	-1001	-1042	-765	-827	-866	-1076	-833	
5	1	-7658	-7895	-7719	-7649	16	19	-7235	-7717	-7719	-7658	-7749	-7827	-7827	-7844	-7859	-7732	-7710	
5	2	8228	7602	7956	7202	53	30	1.9683	7704	7702	7796	7829	8043	8068	8143	8228	8066	8066	
5	3	16155	17614	17958	17800	36	21	2.1747	17655	17614	17975	17922	17683	18076	18155	17940	18005	18005	
5	4	455	32	32	32	32	32	1.3454	32	32	32	32	32	32	32	32	32	32	
5	5	3288	1894	2427	2688	97	62	2.4916	1896	3208	2549	2384	2309	2605	2791	3014	2003	2292	
5	6	6746	1550	2364	2362	313	50	38.6457	1550	1555	2194	2194	1928	2845	2627	6746	2342	2144	
5	7	726	-6	-20	-20	-30	27	36	-5685	-237	-227	-245	-317	-26	-256	-240	-240	-200	
5	8	774	332	537	537	655	40	28	2.0596	306	326	667	522	442	301	577	673	802	577
5	9	-765	-1438	-949	-861	41	47	1.7804	-1096	-1438	-942	-1001	-1042	-765	-827	-866	-1076	-833	
6	1	-2003	-2217	-2071	-2169	16	13	1.3247	-2079	-2217	-2075	-2067	-2149	-2003	-2061	-2184	-2101	-2038	
6	2	42108	4003	40269	40720	77	46	3.7265	4003	40269	40427	40527	4017	40879	40881	40681	404084	40772	
6	3	35711	34949	34076	34071	31	21	2.0250	35711	35711	35711	35711	35711	35711	35711	35711	35711	35711	
6	4	1125	165	795	920	60	26	5.6423	35711	35711	35711	35711	35711	35711	35711	35711	35711	35711	
6	5	5198	1571	2012	2641	94	59	2.5281	1571	2131	2033	1936	1912	1840	3198	2220	1992	1718	
6	6	7068	1707	2486	2492	327	51	39.8069	1781	1781	2077	2077	2154	2700	2886	2190	2392	2392	
6	7	5733	341	996	1266	298	62	22.8905	348	476	872	875	843	1313	1854	1591	1514	869	
6	8	742	-47	-21	-11	31	31	1.3047	-10	-20	-20	-20	-20	-20	-20	-20	-20	-20	
6	9	422	232	537	111	194	37	35	1.1113	55	81	170	102	172	147	422	54	359	413
7	1	29473	29208	29397	29410	20	20	0.9630	29279	29208	29415	29352	29473	29388	29367	29371	29470	29470	
7	2	1831	2810	29170	28170	20	20	0.9630	1931	1931	1931	1931	1931	1931	1931	1931	1931	1931	
7	3	442	6	386	510	40	40	1.3454	3226	3226	3226	3226	3226	3226	3226	3226	3226	3226	
7	4	1854	8	651	1161	121	64	59	2.2082	466	1137	1137	954	679	678	1845	1641	1371	1049
7	5	5026	153	981	1502	300	62	23.2918	153	175	841	95	308	1873	1346	5926	752	938	
7	6	770	-54	-23	-23	40	40	1.3454	-10	-20	-20	-20	-20	-20	-20	-20	-20	-20	
7	7	70	34	86	426	278	50	37	1.0830	306	463	440	420	424	486	667	667	667	667
7	8	261	-70	84	161	32	53	3.3696	100	-191	-409	-72	-221	-180	-41	156	207	79	
9	1	20278	19784	19997	2003C	34	21	2.4511	20271	20100	19984	20034	20278	19784	20278	20017	19840	20091	
9	2	2296	22530	22717	22730	46	34	1.0755	22614	22570	22541	22547	22727	22966	22850	22909	22902	22680	
9	3	18282	17071	17611	18110	30	30	2.0250	18074	17804	17804	17804	17804	17804	17804	17804	17804	17804	
9	4	4165	-91	354	450	59	36	2.6708	231	451	450	169	249	311	168	567	567	567	
9	5	1762	601	1222	1802	84	69	1.4985	737	1282	1157	1264	601	1640	1762	1504	1547	1022	
9	6	4938	543	1052	1203	304	30	2.3216	543	757	912	855	915	908	1175	949	1637	711	
9																			

sponding values in Table 3 are 5.8 and 57.7. The average value for the positional parameters is about 2 and for the thermal parameters about 5. (The mean value should be 1.0,  $\sigma=0.4$ .) Thus, if the agreement among experiments is taken as a criterion of accuracy, the internal estimates of the standard deviations from the least-squares refinements are too low by a factor of  $(\text{RATIO})^{1/2}$ . If any one of the experimenters had reported his least-squares derived standard deviations, a false picture of the accuracy of these parameters could have been presented. The internal standard deviations for positional parameters could be as much as a factor of 2 too small: those for thermal parameters would not infrequently be an additional factor of 2 or 3 too small. It is of course possible that one or more experiments may be more accurate than the others and that the standard deviations reported in such experiments are a reliable indication of accuracy; it is clear however that the average accuracy is not as great as the precision of the individual refinements. Furthermore, the *average* parameter values differ from the OSK values by as much as  $6.4 \sigma_{\text{EXT}}$  for  $O(3)x$  and by  $10.7 \sigma_{\text{EXT}}$  for  $O(4)\beta_{22}^*$ .

\* The mean values in Tables 2 and 3 are probably less accurate than the results of OSK, since the latter are based on data extending to higher scattering angles. On the other hand, there is no reason to assume that the results of OSK are not subject to some systematic error which would render the quoted standard deviations too low by a factor of 2 or 3. Without any evidence to the contrary, the definitive parameters for this structure should be taken as those of OSK rather than any of those quoted here. The estimated  $\sigma$ 's of OSK are much smaller than the  $\sigma_{\text{EXT}}$  in this study.

The maximum variation between a position coordinate determined in an individual experiment and the average value for that coordinate in Table 2 is  $0.043 \text{ \AA}$ .† The maximum variation from the value found by OSK is somewhat larger,  $0.052 \text{ \AA}$ . In terms of the individual standard deviations from the least-squares refinements, such atomic position differences would be considered significant. However, use of a factor of 2 or 3 to obtain a more meaningful standard deviation, as suggested by the comparison between the external and internal estimates, would render most of the differences not statistically significant.

It is instructive to examine the least-squares refined structural parameters based on one group of experiments which were considered to have the best internal consistency as judged by a number of indicators (see part I for details). This *modal* group consisted of experiments 1, 2, 3, 5, 7 and 16. We have already noted that experiment 3 gave divergent results on attempting to refine the parameters for all atoms including hydrogen. In the following, we therefore compare only the *heavy* atom parameters. The results are listed in Table 5 in the same form as Table 2.

Excluding the  $\beta_{ij}$  values for  $i \neq j$ , which are particularly susceptible to anisotropic error, there are 539 different parameter values in Table 5. The range in each parameter value for the *modal* group may also be taken as a measure of consistency. The *average* range for the position parameters is  $11.4 \sigma_{\text{INT}}$ ; for the thermal parameters it is  $16.5 \sigma_{\text{INT}}$ . Individual ranges, of

† Except for experiment 11b, which did not converge.

Table 4. Agreement ratios  $R$  and  $wR$  for the least-squares refinement of the data

$\sigma(x)$  is a typical value of the estimated standard deviation of a positional parameter in the heavy atom refinement.

Experiment number	Heavy atom refinement			Hydrogen atom refinement		Number of reflections* in refinement
	$R$	$wR$	$\sigma(x)$	$R$	$wR$	
1	0.063	0.094	0.0016	†	†	239
2	0.091	0.110	0.0006	0.076	0.091	368
3	0.049	0.060	0.0011	†	†	277
4	0.104	0.127	0.0008	0.089	0.107	331
5	0.034	0.064	0.0003	0.029	0.043	607
6	‡	‡	‡	‡	‡	96
7	0.063	0.077	0.0004	0.047	0.052	429
8	0.079	0.114	0.0007	0.065	0.093	355
9	0.064	0.090	0.0005	0.048	0.066	366
10	‡	‡	‡	‡	‡	129
11a	0.075	0.133	0.0010	0.063	0.123	342
11b	0.097	0.163	0.0022	§	§	164
12	0.112	0.178	0.0016	†	†	403
13	0.057	0.071	0.0006	0.047	0.060	417
14	0.081	0.104	0.0008	†	†	273
15	0.047	0.063	0.0008	0.029	0.039	324
16	0.049	0.070	0.0004	0.034	0.043	429

\* The numbers greater than 332 occurred because of the appearance of equivalent reflections which were not averaged before the refinement.

† Diverged on attempted hydrogen atom refinement.

‡ Insufficient data for refinement.

§ Hydrogen atom refinement not attempted.

|| Did not converge. These were lowest  $R$  factors obtained.

course, are larger with maximum values of  $38 \sigma_{\text{INT}}$  for  $O(1)x$  and  $34 \sigma_{\text{INT}}$  for  $C(2)\beta_{33}$ . The expected value is  $6 \sigma_{\text{INT}}$  for a normal distribution with this number of degrees

of freedom. The frequency with which a given experiment is associated with an extremum of a range for the 539 parameters in question is also revealing, as shown

Table 5. Results of heavy atom refinements for the modal experimental group

For five degrees of freedom, a value of RATIO greater than 2.21 is significant at the 95% level.

ATOM	P	MAXIMUM	MINIMUM	AVERAGE	OSK	SIGMA(EXT)	SIGMA(INT)	RATIO	1	2	3	5	7	16
1	1	33941	33174	33747	33820	49	20	6.0105	33941	33798	33174	.33726	33796	33775
1	2	3430	3430	3430	3430	0	0	0.0000	3430	3430	3430	3430	3430	3430
1	3	51635	50963	51070	51020	69	30	5.2234	51162	51179	51047	51047	51047	51039
1	4	1320	522	786	965	69	33	4.3889	597	522	1320	856	736	740
1	5	2158	1039	1812	2355	129	67	3.7063	2158	1039	1736	2064	1734	1826
1	6	1618	670	1086	1149	97	66	2.1755	1488	670	1618	1183	957	1092
1	7	243	-136	35	-2	26	44	.3590	-136	4	243	11	16	53
1	8	272	-90	243	284	26	34	.5754	64	186	-90	272	252	261
1	9	426	60	348	289	45	65	.4735	60	307	116	426	309	405
2	1	43186	42041	42970	42960	25	19	1.5940	43065	42947	43186	42941	42945	43044
2	2	-3322	-3409	-3249	-3409	39	50	.6100	-3695	-3539	-3322	-3405	-3460	-3325
2	3	-2118	-2467	-2149	-2189	34	29	1.3690	-2169	-2123	-2467	-2118	-2170	-2118
2	4	1103	429	762	725	62	30	4.0544	1103	429	1016	850	769	689
2	5	2864	1511	2301	2713	158	83	3.6170	1927	1511	2864	2590	2135	2172
2	6	1282	682	953	1412	51	61	.6776	682	854	1282	909	955	997
2	7	583	306	367	186	26	47	.3167	395	306	583	369	348	347
2	8	380	159	282	407	26	37	.4736	380	172	159	325	318	231
2	9	-142	-883	-216	-298	85	64	1.7739	-397	-165	-883	-161	-142	-146
3	1	60993	60843	60955	60840	16	21	.6115	60914	60843	60993	60956	60979	60966
3	2	594	227	483	500	45	54	.6812	227	350	410	540	406	594
3	3	30369	30046	30120	30050	27	33	.6774	3052	30046	30369	30107	30592	30140
3	4	929	277	453	578	53	32	2.7177	929	786	476	529	495	
3	5	2073	960	1668	2374	146	62	3.1603	960	1010	2073	1944	1648	1570
3	6	2979	917	1645	1634	159	60	7.0195	917	1064	2979	1818	1621	1549
3	7	236	-193	15	116	36	40	.8225	236	126	-193	4	74	-37
3	8	546	2	160	303	37	41	.8010	546	98	2	191	121	140
3	9	861	149	290	440	64	60	1.1363	194	327	861	333	292	149
4	1	30852	30676	30739	30630	21	20	1.0983	30696	30852	30763	30758	30733	30676
4	2	41985	41357	41683	41730	58	47	1.5442	41357	41423	41885	41706	41589	41780
4	3	23559	23211	23942	23350	29	31	.9064	23211	23258	23599	23567	23546	23547
4	4	645	342	558	648	35	32	1.2581	342	352	645	615	594	545
4	5	1432	646	974	1708	90	63	2.0700	1432	646	1054	1178	859	792
4	6	1671	612	1150	1018	98	57	2.9162	1045	612	1671	1167	1179	1214
4	7	55	-563	-21	-199	49	43	1.2982	-563	55	-176	-5	28	6
4	8	336	227	280	171	19	35	.3012	306	227	289	336	254	245
4	9	181	-49	114	58	20	53	.1515	-49	181	129	128	134	87
5	1	-7674	-8001	-7758	-7649	37	23	2.6114	-8001	-7704	-7922	-7674	-7792	-7821
5	2	8260	7753	7760	7609	57	56	1.0436	8260	7753	7805	8060		
5	3	17954	17716	17802	17900	26	39	.4447	17916	17716	17954	17776	17783	17830
5	4	1239	44	754	640	71	33	4.6110	725	484	1289	829	676	705
5	5	3427	2027	2455	2688	122	100	1.4923	3427	2027	2090	2661	2461	2378
5	6	2715	1355	1973	2362	132	66	3.9988	1504	1355	2775	2056	1949	2020
5	7	38	-547	-293	-380	43	56	.6030	38	-303	-547	-247	-317	-286
5	8	500	-374	419	511	68	39	3.0895	500	321	-374	489	476	402
5	9	-766	-1254	-676	-861	46	78	.3444	-1254	-943	-878	-857	-930	-766
6	1	-2016	-2223	-2054	-2169	22	21	1.0946	-2223	-2040	-2198	-2055	-2016	-2033
6	2	40583	40198	40346	40720	61	59	1.0946	40327	40198	40238	40268	40303	40583
6	3	30536	34659	34982	34610	47	39	1.4402	34744	34925	34659	35033	35036	35017
6	4	848	474	783	920	48	41	1.3867	616	474	839	848	815	800
6	5	3028	1471	2211	2641	173	96	3.2577	1471	1763	3028	2588	2112	2008
6	6	2925	174	223	2492	105	76	1.9081	2925	1764	2725	2330	2111	2206
6	7	-8	-139	-86	-1	22	57	.1514	-94	-118	-69	-139	-98	-8
6	8	623	362	550	655	30	44	.4704	567	428	362	623	536	529
6	9	-37	-1009	-681	-885	83	86	.9409	-1009	-501	-37	-738	-710	-737
7	1	29565	28951	29296	29410	36	32	1.3057	28951	29207	29565	29319	29249	29338
7	2	1684	1156	1525	1590	65	69	.8721	1320	1492	1156	1486	1588	1684
7	3	28290	27476	28173	28320	77	49	2.4415	27684	28177	27476	28290	28227	28137
7	4	1451	109	580	510	104	45	5.2177	1451	109	1355	575	502	732
7	5	2380	963	1551	1411	168	109	2.2513	1490	963	2380	1813	1316	1301
7	6	1478	40	1074	1266	117	86	1.8690	40	995	1478	1184	1179	1041
7	7	437	27	247	111	31	65	.2271	437	160	27	294	211	266
7	8	496	-861	408	194	62	52	1.4184	419	413	-861	496	439	298
7	9	335	-185	-64	161	62	85	.5396	289	92	335	-71	-131	-185
8	1	46498	45867	46327	46400	40	31	1.6406	46498	46448	45867	46318	46349	46297
8	2	-566	-1244	-760	-679	88	59	2.1696	-1041	-1000	-1244	-680	-753	-566
8	3	19385	18822	18930	19110	48	47	1.0266	19115	19024	19385	18851	18847	18822
8	4	1115	39	431	665	80	54	2.1523	54	39	1115	54	54	54
8	5	1812	-27	739	1161	133	94	1.9730	-27	270	1204	54	558	726
8	6	3968	707	1274	1502	185	95	3.8185	876	707	3968	1461	1463	1112
8	7	423	-296	-70	-11	51	57	.8205	423	-161	-294	-122	-21	-33
8	8	337	-1669	227	278	79	57	1.9369	-42	180	-1649	337	311	110
8	9	393	20	151	161	43	84	.2713	231	196	393	20	208	191
9	1	20205	19905	20143	20030	23	29	.6360	19905	20191	20070	20122	20133	20205
9	2	22640	22431	22516	22730	37	67	.5726	22523	22483	22454	22431	22550	22640
9	3	18144	17787	18021	18110	36	48	.5726	17787	18025	18034	17981	17570	18144
9	4	276	-188	149	442	67	42	2.4553	-93	-86	-188	236	276	139
9	5	2213	961	1222	1532	93	86	1.1898	2213	961	1519	1232	1220	1046
9	6	1050	83	800	954	140	82	2.8513	969	220	83	1050	866	884
9	7	-252	-770	-414	-3	62	62	1.0122	-770	-632	-252	-517	-465	
9	8	1468	0	153	142	100	52	3.6037	0	14	1468	52	210	200
9	9	68	-528	-78	33	59	88	.4572	-528	-250	-24	68	-110	-118
10	1	2517	2173	2219	2190	34	32	1.1260	2279	2209	2517	2192	2173	2232
10	2	25638	25189	25242	25280	64	73	.7728	25296	25189	25638	25368	25330	25599
10	3	24917	24744	24914	24960	35	46	.5707	24795	24744	24781	24761	24668	24964
10	4	1722	343	623	496	85	57	2.1689	364	92	1722	1211	1181	1233
10	5	1271	727	1154	1802	59	110	.2961	1253	727	1531	930	940	
10	6	1531	473	881	1203	86	98</td							

below, the italicized value giving the frequency:

	Experiment					
	1	2	3	5	7	16
Maxima:	11	1	31	6	3	7
Minima:	16	27	10	3	1	2

The distribution of the maxima and minima differ significantly from the expected uniform distribution. That experiment 3 accounts for most of the maximum values and experiment 2 for the minimum values is further indication that the *modal* group still contains some systematic errors which are correlated with structural parameters.\*

The low values found for the least-squares derived standard deviations are to be associated with the known systematic errors present in some, if not all, of the experiments. The formulas used to derive the internal standard deviations assume that only random errors are present in the observations. As this condition is increasingly violated, the apparent standard deviation, which is only a measure of the precision of fit between the model and the observations, becomes correspondingly unreliable as a measure of accuracy.

### Conclusion

Systematic differences among structure factors from different experiments and different crystals are manifested in systematically different parameters when the data are subjected to least-squares refinement. Even if the parameters of an acceptable theoretical model re-

\* The large number of extrema for experiment 3 is partially influenced by the fact that, because of the smaller number of reflections, it has larger internally estimated standard deviations. On this basis, the number of extrema should be 3 to 4 times as great as for other members of the modal group.

fine without divergence, the derived parameters may be in error by several times the estimated standard deviations calculated from the goodness-of-fit achieved as a result of the least-squares refinement. Standard deviations on bond lengths and thermal parameters obtained in crystal structure refinements are realistic only if (1) there are no errors in the theoretical model and (2) if there are no systematic errors in the experiment. It is hoped that by projects such as this, the validity of (2) may be assessed so that we may direct our attention toward (1) – which includes all the questions of physical and chemical interest.

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## A Direct Method for the Determination of Polytype Structures. I. Theoretical Basis

BY K. DORNBURGER-SCHIFF

Deutsche Akademie der Wissenschaften zu Berlin, Institut für Strukturforschung, Berlin-Adlershof, Germany (DDR)

AND M. FARKAS-JAHNKE

Research Institute for Technical Physics of the Hungarian Academy of Sciences, Budapest, Hungary

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A direct method for the determination of polytype structures of SiC, ZnS and similar substances from X-ray data is described. It is based on the values of a Patterson-like function (the ‘Pattersonian’) which only depends on the stacking of the translationally equivalent layers of the structure. The way of obtaining the Pattersonian function from the experimental intensities is described and an algorithm given by which the sequence of layers may be deduced. This sequence is conveniently characterized by the sequence of the digits of a binary number. The influence of experimental errors in the intensities on the possibilities of determining the real sequence is discussed.

### Introduction

It has been found recently that optical and electronic data of semiconducting substances, especially of ZnS

and SiC, depend on the polytype present (Kholuyanov, 1964; Gobrecht, Nelkowski, Baars & Brandt, 1965; Hamilton, Patrick & Choyke, 1965; Patrick, 1965; Patrick, Choyke & Hamilton, 1965; Brafman & Stein-